

## FORMULATION

We start by writing the curl of the electric field.

$$\vec{\nabla} \times \vec{e} = -\mu_o \frac{\partial}{\partial t} \vec{h} \quad (4.2)$$

A physical magnetic device must also satisfy  $\vec{\nabla} \cdot \vec{B} = 0$ ,  $\vec{\nabla} \times \vec{B} = 0$  and therefore  $B_{wox}$ ,  $B_{woy}$ ,  $k_w$ ,  $\phi_{wx}$  and  $\phi_{wy}$  cannot be chosen arbitrarily.

$$\begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ 0 & 0 & -jk_o \\ e_x & e_y & e_z \end{bmatrix} = -\mu_o \frac{\partial}{\partial t} \vec{h} \quad (4.3)$$

The matrix form of the curl equation can be written as three separate equations.

$$\hat{x} e_y (-jk_o) = \hat{x} \left( -\mu_o \frac{\partial}{\partial t} h_x \right) \quad (4.4a)$$

$$\hat{y} e_x (-jk_o) = \hat{y} \left( -\mu_o \frac{\partial}{\partial t} h_y \right) \quad (4.4b)$$

$$\hat{z} (0) = \hat{z} \left( -\mu_o \frac{\partial}{\partial t} h_z \right) \quad (4.4c)$$

Substituting  $k_o = \omega_o \sqrt{\mu_o \epsilon_o}$  and  $\eta_o = \sqrt{\frac{\mu_o}{\epsilon_o}}$  and rearranging the terms we can write the equations for the individual components of the magnetic field.

$$\frac{d}{dt}(\eta_o h_x) = -j\omega_o e_y \quad (4.5a)$$

$$\frac{d}{dt}(\eta_o h_y) = j\omega_o e_x \quad (4.5b)$$

$$\frac{d}{dt}(\eta_o h_z) = 0 \quad (4.5c)$$

The curl equation for the magnetic field can also be written in matrix form.

$$\vec{\nabla} \times \vec{h} = \epsilon_o \frac{\partial}{\partial t} \vec{e} - N_o q \vec{v} \quad (4.6)$$

$$\begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ 0 & 0 & -jk_o \\ h_x & h_y & h_z \end{bmatrix} = \epsilon_o \frac{\partial}{\partial t} \vec{e} - N_o q \vec{v} \quad (4.7)$$

Equation (4.8) can be written as three separate equations.

$$\hat{x} h_y (-jk_o) = \hat{x} \left( \epsilon_o \frac{\partial}{\partial t} e_x - N_o q v_x \right) \quad (4.8a)$$

$$\hat{y} h_x (-jk_o) = \hat{y} \left( \epsilon_o \frac{\partial}{\partial t} e_y - N_o q v_y \right) \quad (4.8b)$$

$$\hat{z} (0) = \hat{z} \left( \epsilon_o \frac{\partial}{\partial t} e_z - N_o q v_z \right) \quad (4.8c)$$

After substituting and rearranging as we did before we can write the equations for the individual components of the electric field.

$$\frac{d}{dt}(e_x) = j\omega_o(\eta_o h_y) + \frac{N_o q}{\epsilon_o} v_x \quad (4.9a)$$

$$\frac{d}{dt}(e_y) = -j\omega_o(\eta_o h_x) + \frac{N_o q}{\epsilon_o} v_y \quad (4.9b)$$

$$\frac{d}{dt}(e_z) = \frac{N_o q}{\epsilon_o} v_z \quad (4.9c)$$

Finally the velocity field equation is given as:

$$\frac{\partial}{\partial t} \vec{v} = -\frac{q}{m} \vec{e} - \frac{q}{m} (\vec{v} \times B_w) \quad (4.10)$$

Writing the velocity equation in matrix form we have:

$$\frac{\partial}{\partial t} \vec{v} = -\frac{q}{m} \vec{e} - \frac{q}{m} \begin{bmatrix} \hat{x} & \hat{y} & \hat{z} \\ v_x & v_y & v_z \\ B_{wox} \cos(k_w z + \phi_{wx}) & B_{woy} \sin(k_w z + \phi_{wy}) & 0 \end{bmatrix} \quad (4.11)$$

The matrix equation is written as three separate equations to show the individual velocity components.

$$\frac{\partial}{\partial t} v_x = -\frac{q}{m} e_x - \frac{q}{m} (-v_z B_{woy} \sin(k_w z + \phi_{wy})) \quad (4.12a)$$

$$\frac{\partial}{\partial t} v_y = -\frac{q}{m} e_y - \frac{q}{m} (v_z B_{wox} \cos(k_w z + \phi_{wx})) \quad (4.12b)$$

$$\frac{\partial}{\partial t} v_x = -\frac{q}{m} e_x - \frac{q}{m} (v_x B_{woy} \sin(k_w z + \phi_{wy}) - v_y B_{wox} \cos(k_w z + \phi_{wx})) \quad (4.12c)$$

Now we make following substitutions as in section 2.3

$$\omega_{bx} = \omega_{bwx} \cos(k_w z + \phi_{wx}) \quad (4.13)$$

$$\omega_{by} = \omega_{bwy} \sin(k_w z + \phi_{wy}) \quad (4.14)$$

where

$$\omega_{bwx} = \frac{q}{m} B_{wox} \quad (4.15)$$

$$\omega_{bwy} = \frac{q}{m} B_{woy} \quad (4.16)$$

which gives

$$\frac{d}{dt}(v_x) = -\frac{q}{m} e_x + \omega_{by} v_z \quad (4.17a)$$

$$\frac{d}{dt}(v_y) = -\frac{q}{m} e_y - \omega_{bx} v_z \quad (4.17b)$$

$$\frac{d}{dt}(v_z) = -\frac{q}{m} e_z - \omega_{by} v_x + \omega_{bx} v_y \quad (4.17c)$$

Equations (4.5b), (4.9a), (4.9c) and (4.15a) are the same as (2.7a) through (2.7d). Equation (4.15c) differs from (2.7e) only by the  $\omega_{bx} v_y$  term. This system of equations is taken as a perturbation and gives us the extraordinary waves.

The set of equations (4.5a), (4.9b) and (4.15b) define a system of equations involving  $h_x$ ,  $e_y$ ,  $v_y$  and  $v_z$ . These equations give us the ordinary waves and again there is also the  $\omega_{bx}$  coupling term. Note that if  $\omega_{bx}$  is zero we have the same situation as in chapter two and there is no coupling. The matrix equations of (4.3), (4.7) and (4.11) can be combined into a single matrix

$$\frac{d}{dt} \begin{bmatrix} \eta_o h_x \\ \eta_o h_y \\ \eta_o h_z \\ e_x \\ e_y \\ e_z \\ v_x \\ v_y \\ v_z \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 & -j\omega_o & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & j\omega_o & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & j\omega_o & 0 & 0 & 0 & 0 & \frac{N_o q}{\epsilon_o} & 0 & 0 \\ -j\omega_o & 0 & 0 & 0 & 0 & 0 & 0 & \frac{N_o q}{\epsilon_o} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{N_o q}{\epsilon_o} \\ 0 & 0 & 0 & \frac{-q}{m} & 0 & 0 & 0 & 0 & -\omega_{by} \\ 0 & 0 & 0 & 0 & \frac{-q}{m} & 0 & 0 & 0 & \omega_{bx} \\ 0 & 0 & 0 & 0 & 0 & \frac{-q}{m} & -\omega_{by} & \omega_{bx} & 0 \end{bmatrix} \begin{bmatrix} \eta_o h_x \\ \eta_o h_y \\ \eta_o h_z \\ e_x \\ e_y \\ e_z \\ v_x \\ v_y \\ v_z \end{bmatrix} \quad (4.18)$$

The 9 x 9 matrix can be reduced to an 8 x 8 matrix by removing the row corresponding to equation (4.5c) since these values are all zero. The matrix can also be rearranged to obtain better insight into the coupling terms.

$$\frac{d}{dt} \begin{bmatrix} e_x \\ \eta_0 h_y \\ e_z \\ v_x \\ v_z \\ v_y \\ e_y \\ \eta_0 h_x \end{bmatrix} = \begin{bmatrix} 0 & j\omega_0 & 0 & \frac{N_0 q}{\epsilon_0} & 0 & 0 & 0 & 0 \\ j\omega_0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{N_0 q}{\epsilon_0} & 0 & 0 & 0 \\ -\frac{q}{m} & 0 & 0 & 0 & \omega_{by} & 0 & 0 & 0 \\ 0 & 0 & -\frac{q}{m} & -\omega_{by} & 0 & \omega_{bx} & 0 & 0 \\ 0 & 0 & 0 & 0 & -\omega_{bx} & 0 & -\frac{q}{m} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{N_0 q}{\epsilon_0} & 0 & -j\omega_0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -j\omega_0 & 0 \end{bmatrix} \begin{bmatrix} e_x \\ \eta_0 h_y \\ e_z \\ v_x \\ v_z \\ v_y \\ e_y \\ \eta_0 h_x \end{bmatrix} \quad (4.19)$$

In chapter 2, the solution was split into two problems, where one problem corresponded to x component of the incident wave, and the other problem corresponded to the y component of the incident wave. The individual solutions were then combined by using superposition. We can use the same method in this case, provided that the x component of the magnetic wiggler field is small compared to the y component. We can state this mathematically by letting  $\omega_{bx} \ll \omega_{by}$ . By setting this limitation, the coupling term  $\omega_{bx}$  in 4.19 can be neglected and there is an uncoupling of the two systems allowing us to solve the systems independently however the input to system 2 when system 1 alone is excited is influenced by the coupling. A similar remark applies when system 2 alone is excited. The solution of this problem will be pursued soon.